# Using power coupling efficiency for **Second** Empa **ALD thin film oxides quantification**



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## **Motivation**

Reference materials for GDOES with high oxygen concentrations providing high oxygen signals are hard to find. There is only one conductive oxide commercially available. In nonconductive samples the erosion rate, and therefore the signal intensity, is strongly dependent on the power coupling efficiency. A complete oxygen calibration curve can be obtained by changing only one parameter which influences the power coupling efficiency. In this study Al2O3 discs of varying thicknesses are used to quantify oxygen in ALD thin film oxides. We deposit ALD thin films in our lab with a home built ALD reactor and wanted to know if it is possible to measure the composition of these layers with GDOES.

# Power coupling efficiency

In the RF-GDOES of nonconductive samples, a voltage drop develops inside the material. The voltage transfer coefficient is defined as the ratio between the peak voltage in front of the sample (facing the plasma) and the peak voltage applied to the back of the sample.

The power coupling efficiency therefore depends on the sample capacitance, which is defined by its relative permittivity, its surface and its thickness.

As ceramic discs with equal surface can easily be purchased, we decided to use a set of Al2O3 ceramic discs with varying thicknesses from 0.8 mm to 3.8 mm.

# **Experimental**

GDOES Device: Horiba JY 5000 RF Plasma: Argon Applied Real Power: 40W Pressure: 650 Pa

Profilometer: AltiProbe optical profilometer

### **Calibration Samples:**

Al2O3 ceramic discs Several conductive samples (3 steel, 1 aluminum, 1 conductive oxide, 1 silicon wafer)

## Calibration

All samples were sputtered for the same amount of time, each crater depth was measured by profilometry

- *x* = *measured crater depth* [*um*] *t* = *sputtering time* [*s*]  $\rho = sample \ density \ [g/cm^3]$
- $s = sputtering rate [g/(m^2*s)]$
- d = crater diameter [m]
- *m* = mass erosion rate [ug/s]
- *c* = *element concentration* [*wt%*]
- $m_e = element mass erosion rate [ug/s]$
- U = element Signal [V]



Figure 1: Normalized signal intensities vs. sample thickness



 $s = \frac{\rho * x}{t}$  $d^2 * \pi$ m = s \* -

 $U \propto m_{\rho}$ 

$$m_e = m * 10^6 * \frac{c}{100}$$



Figure 2: Al 396 calibration lines (non- and conductive samples)





# **ALD thin film**

Al calibration line of ceramic samples was used



Figure 7: Raw signals showing interference @ Al 396 due to transparent ALD layer, UV lines show no interference









Figure 3: O 130 calibration line



Figure 5: C 156 calibration line

**Figure 4:** Si 288 calibration line



Figure 6: N 149 calibration line

erage composition between 20 ana 40 sec

Al: 40.2%; O: 59.7%; C: 0%; N: 0.1%; Si: 0%

# Conclusions

Unfortunately the Aluminum calibration line of the nonconductive samples does not fit with the line obtained with conductive samples.

Using Al calibration of the noncoductive samples together with the interference correction provides very good results in quantification of the ALD layers.

Next approach would be to incorporate other ceramics like ZrO2 as well as thinner discs (down to 0.3 mm) to see if there is a similar effect.

## **References:**

Alwyn B. Anfone and R. Kenneth Marcus - Radio frequency glow discharge optical emission spectrometry (rf-GD-OES) analysis of solid glass samples L. Therese, Z. Ghalem, P. Guillot, P. Belenguer - Improved voltage transfer coefficients for nonconductive materials in radiofrequency glow discharge optical emission spectrometry

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